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(54) **Reduction of organically bound chlorine formed in chlorine dioxide bleaching**

(57) The invention relates to an improvement in bleaching of kraft pulp. In ECF bleaching chlorine dioxide is most often a preferred bleaching chemical in certain process positions. The disadvantage is that residual amounts of organically bound chlorine in form of AOX, i.e. organically bound chlorine in effluents, and/or OCl, i.e. chlorine organically bound in the produced pulp, is obtained. A normal approach has been to reduce charges of chlorine dioxide.

According to the invention could substantial reductions in AOX levels be obtained if the process conditions in the chlorine dioxide stage elevated to above 91°C and extended to more than 90 minutes. A major reduction of AOX up to 50% have been shown without a corresponding increase in OCl. The chlorinated substances is degraded by the process conditions to harmless chloride ions, instead of being liberated into the effluent as AOX or bound to pulp as OCl.

Chlorinated organic structure bound to the pulp

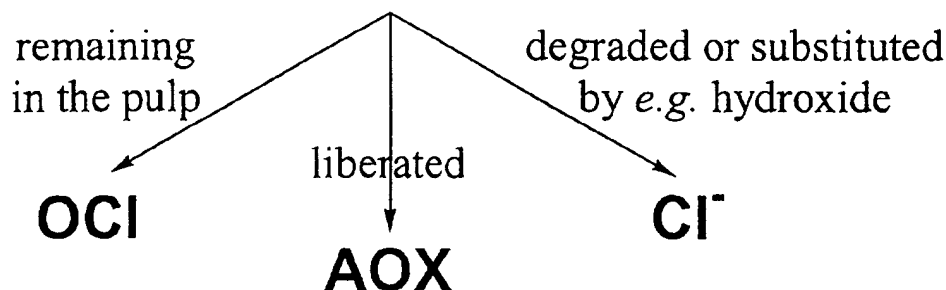


FIGURE 2

Description**BACKGROUND OF THE INVENTION**

[0001] The present invention is related to the formation of chlorinated organic matter in chlorine dioxide bleaching of kraft pulp, and how to reduce the amount of organically bound chlorine in pulp (OCI) and/or reduce the amount of organically bound chlorine compounds (measured as e.g. AOX or TOCI) in the waste water.

[0002] The most efficient and inexpensive bleaching chemical so far known is elemental chlorine, the use of it has in most parts of the world come to an end during the last decade. The driving forces in this development has been environmental, expressed either as market demands or as environmental standards set by governments or a combination of the two.

The negative environmental impact connected to the use of elemental chlorine is primarily the formation of chlorinated organic structures.

[0003] Following a massive introduction of oxygen delignification systems, the work needed in the subsequent bleaching could be significantly reduced and the ECF concept (Elemental Chlorine Free), i.e. bleaching without the use of any elemental chlorine or hypochlorite, was introduced. The chemical normally replacing the elemental chlorine is chlorine dioxide, which had been used for final brightening of pulp and for obtaining a good cleanliness, e.g. due to its excellent capability of removal of extractives.

[0004] The chlorinated structures, e.g. formed in chlorine bleaching, are denoted AOX (adsorbable organic halogene compounds) when found in the bleach effluents and OCI (organically bound chlorine) when stuck in the pulp. The amount of both AOX and OCI were largely reduced upon conversion to ECF bleaching, but a zero level was not reached and in fact a significant amount of OCI is still found in ECF bleached pulps and AOX in the effluents from chlorine dioxide stages.

The levels are also significantly higher than those arising from TCF (Totally Chlorine Free) bleaching operations. This is due to the fact that when chlorine dioxide reacts with the lignin in pulp, hypochlorous acid in equilibrium with chlorine is formed, both of which are able to act as chlorinating agents. Also during manufacturing of chlorine dioxide at the mill site some elemental chlorine is produced, typically in the order of 1-4%, most often below 5% elemental chlorine, all dependent on the type of chlorine dioxide forming process used.

[0005] Considering AOX in effluents it is urgent to keep in mind that although the discharges per ton of pulp produced have decreased significantly when switching to ECF-bleaching, the mills have simultaneously grown too, meaning that the total AOX load to the specific recipient need not have changed very much and thus still constituting a potential problem. In figure 1 is shown how the total amount of AOX in effluents may be constant even though the AOX level per BDt pulp have decreased over time, due to that production volumes have increased.

A pulp having been bleached using chlorine dioxide in an ECF sequence is still easily identified due to its content of OCI, which hinders it from being used in certain paper products or at certain markets. For several mills producing market pulp this is a crucial fact, since it means certain customers will not be interested in a high OCI pulp.

[0006] For various reasons, a massive conversion to TCF bleaching has so far not occurred, leaving the field open for innovative ways to approach the OCI and AOX problems in ECF-bleaching.

[0007] The obvious way, to reduce the overall charge of chlorine dioxide, has in several cases been entered upon in, what is often called "ECF-light" concepts, using a rather small charge of chlorine dioxide in the D-stage, often a charge factor of active chlorine as chlorine dioxide of below 1.

At the Tappi Pulping Conference Oct.22-25, 1989, two papers were presented where solutions to the AOX problem was presented. Lowering of the delignification in the D-stage (or C- or C/D-stage), by using a lower charge factor of active chlorine as chlorine dioxide (i.e. kappa factor) was identified as methods for decreasing AOX, and where compensation for the lower delignification effect in D-stages is made by higher charges in other stages. One paper was presented by J.Basta, L.Holtinger, J.Hook and P.Lundgren with the title "LOW AOX, POSSIBILITIES AND CONSEQUENCES" (pp. 427-436), and the second paper was presented by H.Suss, W.Eul, N.Nimmerfroh and J.Meier, all from Degussa AG/Corp, with the title "ENVIRONMENTAL ASPECTS OF SHORT-SEQUENCE BLEACHING" (pp. 527-537).

The main approach in these papers, when AOX-reduction is the objective in ECF-bleaching, is to decrease the use of chlorine dioxide at the expense of higher charges of hydrogen peroxide.

This approach is shown in EP,B,500813, where a charge factor of active chlorine as chlorine dioxide below 2.0 is used in the D₀ stage (i.e. the first D-stage in a multiple sequence D-E-D... etc.), and where following P-stage (P=peroxide) use at least 3.0 kg of hydrogen peroxide per ton dry pulp, and having chlorine dioxide charges in following D-stages less or equal than the charge used in D₀, i.e. from 20-100% of the D₀ charge.

[0008] In addition to this approach it has been proposed the first chlorine dioxide stage be pH profiled by means of a short-term reaction at low pH followed by an increase to alkaline conditions (Ljunggren, S., Bergnor, E. and Kolar, J. (1994): Modified Modern ClO₂-Bleaching, International Pulp Bleaching Conference (IPBC), Vancouver, Canada, Vol. 1: 169-176. and Ljunggren, S., Bergnor-Gidnert, E. and Kolar, J. (1996): Chlorine Dioxide Bleaching with a Two-

step Low-to-High pH Profile, Tappi J. 79: 12, pp.152-160.).

This approach has many similarities with the Ultim-O process (no washing between D0 and E). Although this approach indeed enabled significant reductions in the AOX discharges, the OCl content was less affected and most important, the need for alkali increased largely, making it less attractive.

- 5 Lately, a reductive alkaline post-treatment has been proposed as a way of significantly reducing the OCl content of a pulp, (see Ljunggren, S., Johansson, E. and Pettersson, B. (1998): Dechlorination of ODEDD Bleached Kraft Pulps, 5th European Workshop on Lignocellulosics and Pulp (EWLP), Aveiro, Portugal, pp. 437-440), which is a somewhat refined way of utilising the well-known fact that an alkali extraction undoubtedly is a very efficient way for the removal of OCl.
- 10 Although efficient, such a post-treatment of the pulp requires both additional washing equipment and additional bleaching towers, making also this approach less attractive for mill implementation.
- [0009] Improvements in Chlorine Dioxide stages have been made for several purposes. In a paper presented by Lachenal, D. and Chirat, C. (1998): High Temperature Chlorine Dioxide Delignification: A Breakthrough in ECF Bleaching of Hardwood Kraft Pulps, Pulping Conference, Atlanta, U.S.A., Vol. 2:pp. 601-604.), a modification of the conventional D-stage is suggested. With the objective to make the D-stage more efficient, and reduce charges of chlorine dioxide, it is proposed to modify the conventional 45°C D-stage to a high temperature (90-100°C) D-stage having long retention time (1.5-4 hrs). An alternative modification achieving the same improvement was proposed where instead this high temperature is implemented after, "at the exit of", the D-stage when the chlorine dioxide have been consumed, during which process position the high temperature could not affect the break-down process of chlorine dioxide in the
- 20 D-stage. This paper also indicates that the change from chlorine to chlorine dioxide bleaching will solve the AOX-problem.

SUMMARY OF THE INVENTION

- 25 [0010] The main objectives with the present invention is to reduce the total amount of chlorinated organic matter leaving a chlorine dioxide stage, and especially the total amount of AOX and OCl, where at least a substantial reduction in AOX levels is obtained, and this while being able to operate chlorine dioxide stages with higher charges of chlorine dioxide than "ECF light".
- [0011] Another objective is that the overall operating costs for pulp bleaching could be kept low if the delignification effect from chlorine dioxide is utilised in full in the first chlorine dioxide stage in the bleaching sequence, whereby charges of other more expensive bleaching chemicals, in cost per kg or per bleaching effect, could be kept at lower levels.
- 30 [0012] Another objective according to the invention is that an initial chlorine dioxide stage run at high temperature for long time is shown to be an efficient means of reducing the overall discharge of AOX by about 50 percent, presumably through a forced degradation of the chlorinated structures formed in the stage. This high reduction of AOX by about 50% at a given overall chlorine dioxide charge compared to operation of said initial chlorine dioxide stage at conventional conditions, i.e. some 60-70°C and 20-60 minutes.
- 35 [0013] Moreover, a further addition of sulphamic acid to a final D-stage is presented as an efficient tool for reducing the total amount of AOX and OCl, with substantial decrease of the OCl content of an bleached pulp, preferably ECF bleached pulp, since sulphamic acid captures *in situ* formed elemental chlorine. Said substantial decrease amounting to about 50 percent in a final D-stage operating at similar charge of chlorine dioxide.
- 40

DETAILED DESCRIPTION OF THE INVENTION

- 45 [0014] The invention is based upon the origin of OCl and ways to decrease it, without necessarily reducing the use of chlorine dioxide and still reaching the same final brightness.
- The distribution of OCl in ECF-bleached pulp is playing an important role.
- [0015] It is important to understand the correspondence between AOX and OCl. In Fig. 2, the three major possible fates of a chlorinated substance in the pulp are summarised. Following a chlorination there are thus three alternatives, either that the chlorinated structure sticks to the final pulp becoming OCl, or that it is liberated during subsequent bleaching stages becoming AOX, or that the structure is substituted/degraded so that the chlorine atoms form harmless chloride ions.
- 50 Important to keep in mind is hence that there is no direct correspondance between AOX and OCl telling e.g. that a high AOX discharge means a low OCl content in the pulp at a certain chlorine dioxide charge.

5-stage sequence trials

- [0016] In a series of trials the standard ECF bleaching sequence of DEDED, using an overall chlorine dioxide charge

of 29.6 kg a Cl/BDt, was used to bleach the oxygen delignified HW kraft pulp from the second series of trials (kappa 9.8) to full brightness (above 89 % ISO). 19.6 kg a Cl/BDt was used in D0, and 5 kg a Cl/BDt in each of D1 and D2. The charge factor of active chlorine as chlorine dioxide in D0 equaling $(19.6/9.8=) 2.0$

This standard sequence was compared with three modified sequences, D*EDED, DEDE(SD) and D*EDE(SD).

- 5 D* denotes a D-stage run at high temperature (90 °C) and long time (120 min). "S" denotes the presence of sulphamic acid. E stages were performed according to above. D1 and D2 stages were performed at 75 °C and 120 min.

General methods

- 10 [0017] Kappa number, viscosity and ISO brightness were analysed using the respective SCAN standards. In addition, SCAN standard CM 52:94 "Pulps, papers and boards - organic chlorine" was used to determine the content of OCl in the pulp after different stages.

- [0018] All bleaching experiments were performed at 10 percent pulp consistency in plastic bags, which after intense kneading were placed in heated water baths. The charge of sulphamic acid should be somewhat higher, *i.e.* on a molar basis; than the charge of active chlorine, in this investigation meaning 1.0 mmol sulphamic acid/BDt.

- 15 [0019] In those stages to which sulphamic acid addition was made, the charge of active chlorine was increased in order to compensate for the decreased oxidising capacity of the stage when the reduction of chlorine dioxide to chloride ion is broken at the level of elemental chlorine. The oxidising capacity of chlorine dioxide is decreased by 20 percent in the presence of sulphamic acid, which captures intermediately formed elemental chlorine, and following reaction pattern is developed with and without sulphamic acid.



- 35 [0020] In practise this means that 4 out of 5 electrons are used when chlorine dioxide bleaching in the presence of sulphamic acid is used and thus the charge of active chlorine to such stages were increased by 25 percent. This way, all the pulps were subjected to identical charges of "active" active chlorine.

Ways to obtain a low OCl pulp and to reduce AOX discharges

- 40 [0021] Results from the 5-stage bleaching study on HW mill oxygen delignified kraft pulp are given in following table 1.

Table 1

45

Trial	DEDED	D*EDED	DEDE(SD)	D*EDE(SD)
final kappa	2.1	0.6	2.5	1.2
final viscosity [ml/g]	975	937	939	911
ISO brightness [%]	89.4	89.9	89.4	89.5
total a Cl charge [kg/ADt]	27	27	27	27
total OCl [mg/kg]	152	158	88	116
total AOX [kg/ADt]	0.41	0.23	0.39	0.21

50

- 55 [0022] From the results it is clear that the AOX discharge could be reduced with about 50 percent using D* instead of D as the first bleaching stage. It should be noted that this result is obtained when comparing sequences with identical overall charge of chlorine dioxide. In addition to this reduction of AOX, the value can be even further reduced when the chlorine dioxide saving effect of the D*, (as *e.g.* noted by Lachenal, D. and Chirat, C (1998): High Temperature Chlorine Dioxide Delignification: A Breakthrough in ECF Bleaching of Hardwood Kraft Pulps, Pulping Conference,

Atlanta, U.S.A., Vol. 2: 601-604.) is taken into account, here instead recorded as a higher final brightness.

[0023] This finding was very unexpected. One would else have anticipated that if the AOX levels experienced a decrease, then the OCl would increase by a similar order. However, the findings showed that the AOX-levels was decreased without a similar order of increase in OCl.

The interpretation of the result should not be that less chlorination takes place or that less AOX is formed in a D*-stage than in a conventional D-stage. On the contrary it seems appropriate to suppose that under the tough conditions of the D* stage, a substantial part of the AOX formed in the stage is further degraded to *e.g.* harmless chloride ions. With this knowledge in mind it is interesting to compare D* with (AD), *i.e.* where A is performed as a hot acid treatment for long duration at *e.g.* 90-100 °C and 120 min according to concepts like GB 1.062.734. In GB 1.062.734 this acid treatment at pH 2.25, temperature 100°C and during 120 minutes was implemented in order to reduce brightness reversion.

The extreme A-stage was followed by a conventional DO-stage at some 60°C without intermediate washing. In conformity with D*, an (AD) approach gives a potential to reduce the overall need for chlorine dioxide in the bleaching of especially HW kraft pulp, although D* has been shown to have a greater potential in this respect. However, in contradiction to D*, an (AD) approach will not enable any reduction of the AOX according to the mechanisms presented. Theoretically, D* can of course be utilised in any position in the bleaching sequence irrespective of the number of D-stages in the bleaching line. Although in general it is likely that the benefits of the stage primarily motivates its utilisation in the D0 position, *i.e.* the first stage using chlorine dioxide.

[0024] From the results in Tabel. 1 it is also clear that the presence of sulphamic acid in the final D-stage is an efficient means of reducing the OCl content of the pulp. Having the OCl pattern shown in Fig. 3 in mind, it is easily concluded that the largest effect to the lowest charge of sulphamic acid is obtained when sulphamic acid addition is made to the last D-stage, although a larger effect of course can be obtained using it in all D-stages. Although sulphamic acid already today is commonly used in pulp mills, *e.g.* for the removal of scales in machinery upon shut-downs, its use in continuous bleaching processes for obtaining low OCl pulp is new. The addition of sulphamic acid should be added in a continuous manner during the bleaching process in the chlorine dioxide stage, *i.e.* so that sulphamic acid is present during the consumption of chlorine dioxide in the chlorine dioxide stage. The sulphamic acid could be added to the pulp before, after or during addition of the chlorine dioxide in a chlorine dioxide mixer.

[0025] It should be added that the chlorine dioxide charge in a (SD) stage has to be increased by some 15-30%, typically 25 percent, in order to compensate for the reduced oxidising power lost due to the capture of elemental chlorine by sulphamic acid. However, when utilised in D2-position, or in the final D-stage, this means a very moderate additional need for chlorine dioxide in this last stage.

[0026] The two concepts D* and (SD) could also be utilised in the same sequence, thus enabling the manufacture of a pulp with low OCl content at the same time as the AOX discharges are kept low, as shown in Tab. 1.

[0027] It can be concluded that a 50 percent reduction of the overall AOX discharge of a DEDED sequence can be obtained by using a D*-stage instead of a conventional D-stage in D0 position.

The OCl content can also be fought and decreased by about 50 percent even in an existing bleaching line by changing the last D-stage to operation with sulphamic acid addition in a (SD)-stage.

Claims

1. A process for reducing the amount of organically bound chlorine formed in chlorine dioxide bleaching of kraft pulp using several bleaching stages and wherein at least one of the stages is a bleaching stage using chlorine dioxide as bleaching chemical, said bleaching stages forming a bleaching sequence, wherein a first chlorine dioxide bleaching stage used during the bleaching sequence is having a charge factor above 0.5 **characterised in that** the first chlorine dioxide bleaching stage used during the bleaching sequence is operated at a temperature above 91°C and at a retention time more than 90 minutes, whereby the resulting AOX content in the effluent from the bleaching line is reduced more than 25 %.
2. A process according to claim 1, **characterised in that** the that the first chlorine dioxide bleaching stage used during the bleaching sequence is operated at a temperature above 95°C up to 120°C at the most and at a retention time more than 90 minutes up to 300 minutes at the most, and preferably about 200 minutes, and that the first chlorine dioxide bleaching stage is pressurised to a pressure exceeding the vapour saturation pressure for the temperature in the stage by at least 20%.
3. A process according to claim 1 or 2, **characterised in that** the charge factor in the first chlorine dioxide bleaching stage is above 1.5 and preferably in the range 1.5-3.0.

EP 1 270 805 A2

4. A process according to any of claims 1-3, **characterised in that** the pulp concentration during the the first chlorine dioxide bleaching stage is in the medium consistency range, i.e. between 7-25%.
5. A process according to any of claims 1-4, **characterised in that** the pulp being bleached in the first chlorine dioxide bleaching stage is delignified to a kappa number below 20, and preferably below kappa 15 prior to bleaching in the first chlorine dioxide bleaching stage.
6. A process according to claim 5, **characterised in that** sulphamic acid is added to at least one chlorine dioxide bleaching stage in the bleaching sequence, which sulphamic acid captures intermediately formed chlorine, or hypochlorite, during the chlorine dioxide bleaching stage forming chlorosulphamic acid according to the reaction process.
7. A process according to claim 6, **characterised in that** sulphamic acid is added to at least one chlorine dioxide bleaching stage in the bleaching sequence in an amount exceeding that of the charge of active chlorine based upon a mmol relation.
8. A process according to claim 6, **characterised in that** sulphamic acid is added to at least one chlorine dioxide bleaching stage in the bleaching sequence in an amount exceeding 1.0 mmol sulphamic acid/BDt of pulp.
9. A process according to claim 6, **characterised in that** the major part, i.e. more than 80% of total charge and preferably 100%, of the total charge of of sulphamic acid added to the bleaching sequence is added to the last chlorine dioxide bleaching stage.
10. A process according to claim 9, **characterised in that** the last chlorine dioxide bleaching stage is at least a D2 stage, i.e. a chlorine dioxide stage preceeded by at least a D0 stage, i.e. the first chlorine dioxide stage, and a D1 stage, having extraction stages between chlorine dioxide stages, i.e. according to a D0-E-D1-E-D2 bleaching sequence.
11. A process according to claim 8,9 or 10 **characterised in that** the charge of chlorine dioxide used in the stage where sulphamic acid is added is increased by at least 10%, preferably increased 20%, as compared to a charge of chlorine dioxide used in this stage without addition of sulphamic acid and resulting in a final pulp brightness in the same order of ISO brightness, i.e. the same order of ISO brightness corresponing to $\pm 1\%$ in final ISO brightness.

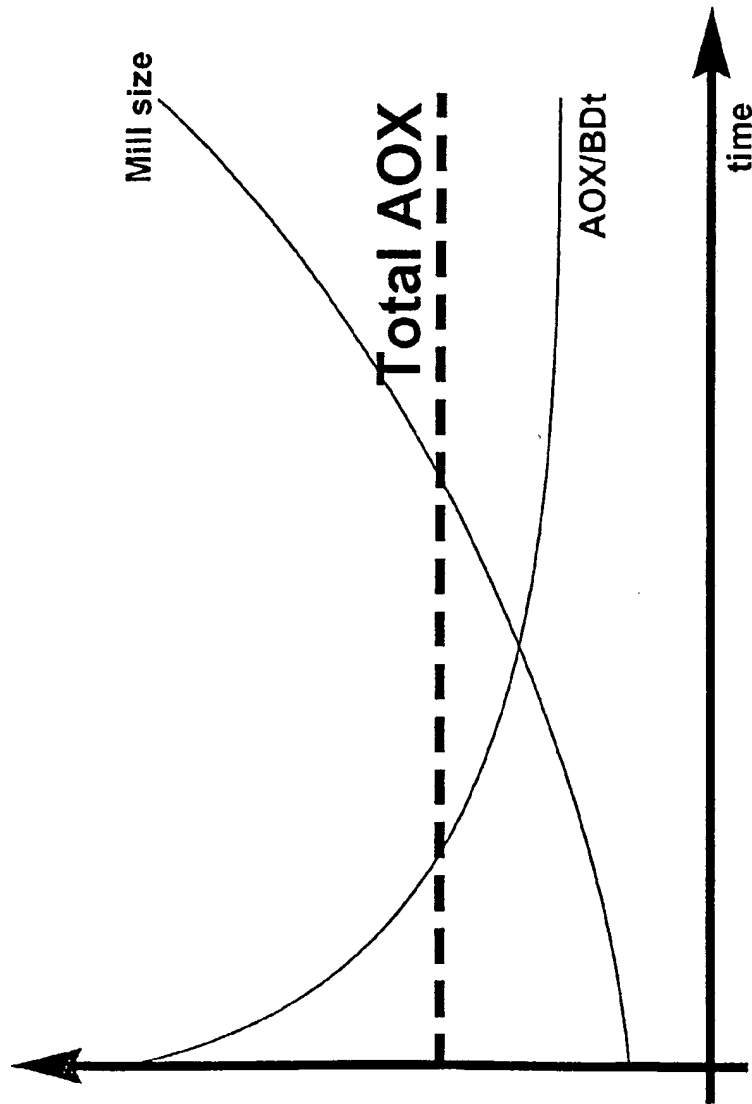


FIGURE 1

Chlorinated organic structure bound to the pulp

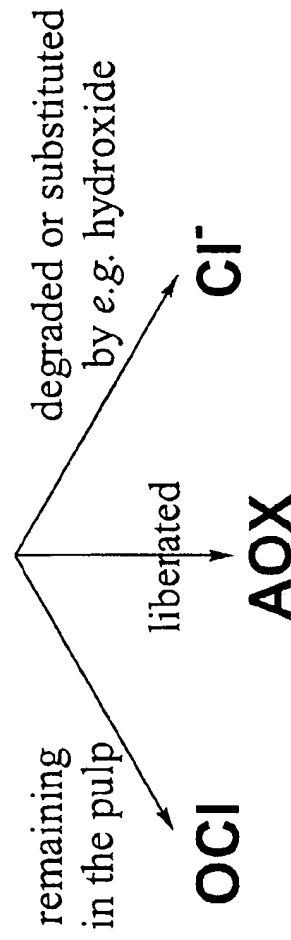
**FIGURE 2**



FIGURE 3



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According to the invention could substantial reductions in AOX levels be obtained if the process conditions in the chlorine dioxide stage elevated to above 91°C and extended to more than 90 minutes. A major reduction of AOX up to 50% have been shown without a corresponding increase in OCl. The chlorinated substances is degraded by the process conditions to harmless chloride ions, instead of being liberated into the effluent as AOX or bound to pulp as OCl.

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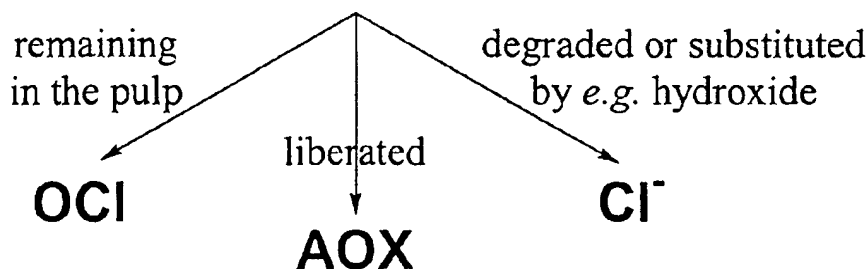


FIGURE 2



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 02 07 6282

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
X	US 3 622 444 A (ANDREWS DOUGLAS HAIG) 23 November 1971 (1971-11-23) * column 1, line 3 - column 2, line 64; examples 1,2 *	1,4	D21C9/14
X	WO 98 00602 A (SUNDS DEFIBRATOR IND AB ;GERMGAARD ULF (SE); MELLANDER PIA (SE); B) 8 January 1998 (1998-01-08) * the whole document *	1,2,4	
A	US 6 235 154 B1 (MCK BERRY RICHARD ET AL) 22 May 2001 (2001-05-22) * column 1, line 28 - line 47 *	6-9,11	
A	US 3 652 388 A (CROON INGEMAR LISS-ALBIN ET AL) 28 March 1972 (1972-03-28) * the whole document *	1	
D,A	EP 0 500 813 B (EKA NOBEL AB) 7 December 1994 (1994-12-07)		
The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
			D21C
Place of search	Date of completion of the search	Examiner	
MUNICH	23 December 2002	Nestby, K	
CATEGORY OF CITED DOCUMENTS		T: theory or principle underlying the invention E: earlier patent document, but published on, or after the filing date D: document cited in the application L: document cited for other reasons A: technological background O: non-written disclosure P: intermediate document &: member of the same patent family, corresponding document	
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**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 02 07 6282

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23-12-2002

Patent document cited in search report		Publication date	Patent family member(s)		Publication date
US 3622444	A	23-11-1971	CA	864409 A	23-02-1971
			ZA	7002034 A	24-11-1971
WO 9800602	A	08-01-1998	SE	506938 C2	02-03-1998
			AU	3468797 A	21-01-1998
			EP	0909354 A1	21-04-1999
			SE	9602602 A	29-12-1997
			WO	9800602 A1	08-01-1998
US 6235154	B1	22-05-2001	AU	2822099 A	11-10-1999
			BR	9908832 A	21-11-2000
			CA	2321683 A1	23-09-1999
			WO	9947744 A1	23-09-1999
			EP	1070167 A1	24-01-2001
			JP	2002506935 T	05-03-2002
US 3652388	A	28-03-1972	SE	334286 B	19-04-1971
			AT	292443 B	25-08-1971
			DE	1959118 A1	11-06-1970
			FI	45573 B	04-04-1972
			FR	2025415 A5	11-09-1970
			NO	130776 B	28-10-1974
EP 0500813	B	02-09-1992	AT	115208 T	15-12-1994
			AU	7235691 A	21-08-1991
			BR	9105959 A	13-10-1992
			CA	2074715 A1	01-08-1991
			EP	0500813 A1	02-09-1992
			ES	2065007 T3	01-02-1995
			FI	923420 A	29-07-1992
			JP	6072385 B	14-09-1994
			JP	4507118 T	10-12-1992
			NO	922995 A	15-09-1992
			PT	96630 A ,B	15-10-1991
			SE	9000340 A	01-08-1991
			WO	9111554 A1	08-08-1991

EPO FORM P0459

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